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TECHNICAL REPORT THREE: MECHANICAL SYSTEMS EXISTING CONDITIONS EVALUATION



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Executive Summary

This report is an examination of the currently existing mechanical system in the NEOMED Research and Graduate Education building and the Comparative Medical Unit expansion. It includes initial design conversation and discussion, load and other calculations, basic system breakdown, and evaluation of cost, space, and LEED certification potential.

Based on the analyses that follow, the top priority of the owner appear to be maintaining a topnotch research and education facility with flexibility and accessibility for students and staff. Considerations for energy efficiency and cost are absolutely made, but do not interfere with established operations and programming.

Building Overview

The project is comprised of three additions to the NEOMED campus. The main addition is the Research and Graduate Education Center, a four-story 63,000 square foot biomedical research building. The first three floors are fully built out with laboratories, support rooms, and offices, while the top floor is shelled in and will be built out as the research program grows. There is a 6,000 square foot basement to house stand-alone utilities.

The second component is a 14,500 square foot addition to the Comparable Medical Unit, which provides animal care services. Lastly, several existing laboratories in Building D were renovated.

Early Design Criteria

Objectives and requirements

The new Research and Graduate Education Building was built to help the university address the biomedical research and education needs of the region. It provides a working space for 30+ scientists focused on research involving better diagnosis and treatment of arthritis, cardiovascular disease, Alzheimer's disease, and innovative ways to design and deliver new medicines. The facility provides full support for teams with offices for faculty, write-up areas for researchers, small group teaching rooms, and open lab and support spaces. The top floor is shelled out for future program expansion.

The existing Comparative Medical Unit provides animal care services for research and teaching programs at the university. It is staffed by 8 personnel under a qualified vet specializing in lab animal medicine. The addition to the existing building was meant to expand animal care capabilities by adding to the vivarium and providing additional mechanical space.

Due to the sensitive nature of the activities in the lab and vivarium spaces, 100% outdoor air is required for these areas. As a result of this requirement, serious thought was given to the different energy recovery measures that could be taken to minimize the energy use of airside systems. HVAC System design was intended to have following characteristics: modular approach, energy responsiveness, flexibility for future changes, durability and ease of maintenance, reliability, and redundancy of critical components.

Code requirements that were followed include:

- Ohio State Building and Mechanical Codes.
- NEOUCOM Design and Engineering Guidelines
- Recommendations of the National Fire Protection Association (NFPA), in general, and, in particular:
 - HVAC: NFPA 90A, 90B, 96
 - HVAC: NFPA 45
- Recommendations of ASHRAE including ASHRAE 62-1999, Indoor Air Quality and ASHRAE/ANSI 15, Chiller Mechanical Rooms.
- National Electrical Code (NEC)
- Energy Conservation Act 222
- ANSI Z 9.5
- USGBC LEED Criteria
- NIH Design Requirements Manual
- Recommendations of AAALAC (animal areas)

Outdoor design conditions

The project is located in Rootstown, Ohio, which ASHRAE places in region 5A-cool and moist. The project mechanical system was designed with a winter exterior design temperature of 0 degrees F and a summer exterior design temperature of 89 degrees dry bulb/73 degrees wet bulb +- 2 degrees.

Indoor design Conditions

Indoor design temperature and humidity varies based on space type. Labs and support spaces are set to 72 degrees F year-round. Mechanical and electrical rooms are conditioned to 65 degrees during the winter and ventilated with no conditioning in the summer. Animal holding rooms in the CMU have a selectable range from 68-85 degrees to provide species-appropriate conditioning, with the exception of rabbit holding areas set to exactly 65 degrees.

Humidity in the lab and associated support spaces is set to $35\%(\pm 5)$ in the winter and $50\%(\pm 5\%)$ in the summer. Vivarium spaces in the CMU are set to $30-40\%(\pm 5)$ during winter and $50\%(\pm 5\%)$ during summer.

Available utilities and rates

Campus utilities include electric, natural gas, cold water and sanitary/storm sewer. Electrical service consists of a high voltage loop stepped down to 480/277 and 208/120 at each building. Site natural gas piping is a mix of low pressure and medium pressure.

With regards to heating, roughly 6 or 8 boiler plants are located at various points on the existing campus. Typically one "heating" location is present for a heating water loop for each building project. The largest of these is the existing boiler and chiller plant in the M building, just to the east of existing CMU. This main plant feeds all of the original 1974 part of campus. The chillers at M Building feed nearly all of the entire campus as well. There are some smaller DX cooling units scattered throughout the campus, but they are not a significant percentage of the campus cooling capacity.

In addition to chillers and boilers, Building M also contains a high pressure steam boiler plant that makes 80 psig steam. Originally a coal fired plant in 1974 with two large coal boilers, it was switched to four natural-gas fired Ohio-Special steam boilers in 1991. The steam plant once served heat exchangers in the M building boiler room, AHU heating coils throughout campus, the DHW tank in the M building, numerous humidifiers throughout campus, and many lab steam outlets, plus steam sterilizers. The NEOMED campus has since downsized their use of steam, and now only hi-pressure steam is distributed to the CMU vivarium equipment, humidifiers in the CMU, and steam sterilizers.

Design influences

Operability was a major influence in initial design, and is one of the factors that drove the decision to provide stand-alone utilities for the RGE Building. The RGE is intended to be available 24/7 to the scientists and their teams, and also the CMU must be able to provide 24/7 HVAC for the animals in the vivarium.

Distance to existing utilities also drove the decision to include stand-alone utilities. Originally, the design team considered extending the hi-pressure steam from the existing M building boiler room to the new RGE building, but that was cut due to budgetary concerns. Space was reserved in the RGE lab AHUs for humidifiers to be installed later, along with space for a medium pressure steam boiler in RGE basement. Also, the design team looked at extending piping from the central M building boiler and chiller plant; however, there was still going to be a need for additional chilled water and heating capacity so the cost to just include a new plant was very similar. Direct burial was considered as well as an indoor route, but that was complicated by the fact that the bridge connectors were alternate bids. The CMU addition is however connected to the M building boiler and chiller plant as well as the steam plant, seeing as the existing utilities were already located in the original building.

A variable air volume was deemed the safest and most obvious choice for airside systems. Due to the very stringent air change per hour requirements and variety of unique spaces, plus the need for 100% outdoor air, custom air handling units were created for the RGE labs and Vivarium expansion. The office side of the RGE does include a custom 30% outdoor air unit with a mixing plenum and economizer for some energy recovery.

Heat and energy recovery was a critical design point due to the large air turnover rate; a number of options were weighed. Desiccant dehumidification was ruled out, primarily due to the chemicals and contaminants that would be present. The design team did not know how those would have reacted with the desiccants, so they erred on the safer side. Also, the additional efficiency would primarily occur during cooling season and in a cool wet climate it was not "where the money was" with savings. Air-to-air, wheel, and heat-pipe systems were all eliminated as energy recovery systems due to their potential cross-over for contamination. A heat-pipe recovery was briefly considered, but would have needed to be a two coil design which is a more complex and expensive variety. The only options left were either simple runaround glycol coils or a heat pump between the outside air and exhaust air streams. The design team elected to use glycol coils in the end.

With concern to controls, the team did not consider CO2 monitoring since most spaces were going to have occupancy sensors; some of the sensors unfortunately did get value-engineered out. The new addition has an automatic temperature control system consisting of an independent direct digital control circuit. This circuit is connected and interfaced with the existing campus front ends to allow the campus-wide system to trend recording of the major equipment operation and alarms. This data is used to develop a point schedule for the RGE, as well as to trend recording of environmental conditions and lighting in the CMU to maintain AAALAC accreditation.

A RO/DI water system was provided for the labs and vivarium spaces, sized to supply the feed for the animal watering equipment. A separate laboratory waste collection system was provided to drain all laboratory fixtures. The waste is piped through a duplex limestone chip tank neutralization system.

With regards to fire protection, the new RGE includes a combination wet sprinkler and standpipe system with sprinkler drain risers extended to spill to the exterior. It was important to specify non-ferrous piping and components to be used in areas subject to magnetic fields or equipment. In addition, a new fire pump room was provided in the RGE basement. The existing CMU building was non fire suppressed, so the new addition was designed to remain non fire suppressed with the inclusion of fire separation walls between the existing building and new addition.

Engineering calculations

Ventilation Rates

Designer ventilation rates were only necessary for the RGE office AHU, given it is the only one that does not rely on 100% outdoor air. Designer calculation could not be located.

Heating and Cooling Loads

Designer calculation are summarized in Appendix A

Annual Energy Consumption

At this point in time, energy meter readings and utility bills are not available

System Breakdown

Air

To achieve proper ventilation and space conditioning, there are five total air handling units for the project, broken down in the table below. AHU-1 and AHU-2 are located on the rooftop of the RGE and serve the Lab and Support areas, while AHU-3 is located on the roof as well and serves the RGE offices. AHU-4 is located in the Basement of the RGE and serves to simply provide constant volume ventilation and space conditioning to the mechanical plant.

	Air Handling Units															
					Fans									Co	ils	
					Supply Return Exhaust					Hea	nting	Coc	oling			
NO.	Type	Area	Min. OA. CFM	NO.	CFM/fan	ESP	NO.	CFM/fan	ESP	NO.	CFM/fan	ESP	GPM	Tot. MBH	GPM	Tot. MBH
AHU-1	Custom VAV	RGE Labs	50,000	4	12,500	4.0"	-	-	-	2	50,000	4.75"	140	2085	470	3584
AHU-2	Custom VAV	RGE Labs	50,000	4	12,500	4.0"	-	-	-	2	50,000	4.75"	140	2085	470	3584
AHU-3	Custom VAV	RGE Offices	8,400	2	14,000	3.0"	1	28,000	2.0"	-	-	-	51	820	150	1294
AHU-4	Constant	RGE Basm.	450	1	4,500	1.0"	-	-	-	-	-	-	13	194.4	47	187
AHU-5	Custom VAV	CMU exp.	85,000	4	21,250	4.0"	-	-	-	3	42,500	4.0"	270	3420	625	6135

	Boilers											
NO.	Туре	Medium	MBH In	MBH out	GPM	Steam PSIG	Min. Gas input pressure					
B-1	Condensing	HW	3,000	2,883	225	-	3.5"					
B-2	Condensing	HW	3,000	2,883	225	-	3.5"					
B-3	Condensing	HW	3,000	2,883	225	-	3.5"					
B-5	Firetube	Steam	1,969	1,697	-	80	9.5"					
B-6	Modulating, Condensing	HW	3,000	2,664	133	-	3.5"					
B-7	Modulating, Condensing	HW	3,000	2,664	133	-	3.5"					

Hot water

			Hydronic Pumps			
	NO.	Туре	Service	GPM	Head Pressure (FT H20)	MHP
	HWP-1	End Suction	Primary Heating Water	450	72	15
	HWP-2	End Suction	Primary Heating Water	450	72	15
	CWP-1	End Suction	Chilled Water Pump	680	65	20
	CWP-2	End Suction	Chilled Water Pump	680	65	20
	TWP-1	Horiz. Split Case	Tower Water Pump	1275	65	30
	TWP-2	Horiz. Split Case	Tower Water Pump	1275	65	30
RGE	HGRP-1	End Suction	AHU-1 Heat Recovery Coil	480	65	15
	HGRP-2	End Suction	AHU-2 Heat Recovery Coil	480	65	15
	HCP-1	In-line	AHU-1 Heating Coil	140	15	1
	HCP-2	In-line	AHU-2 Heating Coil	140	15	1
	HCP-3	In-line	AHU-3 Heating Coil	50	12	0.5
	HCP-4	In-line	AHU-4 Heating Coil	12	12	0.125
	CWP-3	In-line	AHU-4 Cooling Coil	47	25	0.75
	HWP-1	End Suction	Heating Water	500	50	15
CMU	HWP-2	End Suction	Heating Water	500	50	15
CIVIO	HCP-1	In-line	AHU-5 Heating Coil	270	12	1.5
	HGRP-1	End Suction	Heat Recovery	540	65	15

Steam

Chiller water

			Chillers		
NO.	Туре	Tons Output	Min. Turndown Tons	Evap. GPM	Cond. GPM
CH-1	Centrifugal	425	45	680	1275
CH-2	Centrifugal	425	45	680	1275

	Cooling Towers											
Motors												
NO.	Туре	Tons	No. Cells	Total GPM	HP	RPM						
CT-1	Crossflow	425	1	1275	25	1800						
CT-2	Crossflow	425	1	1275	25	1800						

Energy Recovery

System Assessment

Initial cost

The rough estimate for the up-front costs of the mechanical system are tabulated below in Table ____. The total budget for all mechanical work wound up at roughly \$6.6 million out of a total project cost of roughly \$40 million.

DESCRIPTION	QUANTITY	UNIT	UNIT PRICE	ESTIMATE	TOTAL
FIRE PROTECTION		\$/SF	\$3.44		\$217,000
PLUMBING		\$/SF	\$21.00		\$1,323,000
HVAC		\$/SF	\$80.94		\$5,099,000

Space utilization

Due to the inclusion of a rooftop penthouse and utility basement, interference with the plan of the RGE was kept to a minimum. Roughly 6000 square feet of basement was used for the Mechanical plant. With the addition of roughly 1090 square feet lost to mechanical shaft space, the project only lost about 7100 square feet to the mechanical system. It is important to note however, that a large ceiling space was included due to big ductwork- a 3 foot plenum that results in a 14'8" floor-to-floor height. Negligible space was lost in CMU addition due to the inclusion of a penthouse, use of existing utilities, and the absence of shafts.

LEED Analysis

The project schematic design outline states that the team sought for a basic LEED Certification level. What follows is a quick breakdown of the RGE and CMU's adherence to the Energy and Atmosphere and Indoor Environmental Air Quality sections of the USGBC LEED 2013 Standard for New Construction.

Energy and Atmosphere Credits

EA Prerequisite 1: Fundamental Commissioning and verification- pass

Commissioning performed by PSI, INC

EA Prerequisite 2: Minimum Energy Performance- pass

Option 2- follows ASHRAE Standard 90.1

EA PREREQUISITE: BUILDING-LEVEL ENERGY METERING-pass

New meters installed for natural gas, HW, DCW, CW, Electric at CMU; meters for NG, Electric, and DCW at RGE

EA PREREQUISITE: FUNDAMENTAL REFRIGERANT MANAGEMENT-pass

No CFC's in any of new construction

EA CREDIT: ENHANCED COMMISSIONING-0 pts

No follow-up commissioning after building opened

EA CREDIT: OPTIMIZE ENERGY PERFORMANCE-0 pts

No energy modeling/simulation performed

EA CREDIT: ADVANCED ENERGY METERING-1 pt

Meters are interfaced with campus network. ATC stores data and trends and develops point schedule

EA CREDIT: DEMAND RESPONSE-0 pts

No demand response program used

EA CREDIT: RENEWABLE ENERGY PRODUCTION-0 pts

No renewable energy sources on campus utilized

EA CREDIT: ENHANCED REFRIGERANT MANAGEMENT- 0 pts

No analysis performed on refrigerants used

EA CREDIT: GREEN POWER AND CARBON OFFSETS-0 pts

No contract engaged

Indoor Environmental Quality Credits

EQ PREREQUISITE: MINIMUM INDOOR AIR QUALITY PERFORMANCE-pass

Project meets ASHRAE STD 62.1

EQ PREREQUISITE: ENVIRONMENTAL TOBACCO SMOKE CONTROL-pass

Due to the nature of the activities inside of both the RGE and CMU, smoking is prohibited in or around

EQ CREDIT: ENHANCED INDOOR AIR QUALITY STRATEGIES- 1 pt

Pressurized Vestibules are used at all entryways, areas with potentially hazardous chemicals are kept at negative pressure and sufficiently exhausted, and all AHU's have MERV-14 after filters

EQ CREDIT: LOW-EMITTING MATERIALS- Opts

EQ CREDIT: CONSTRUCTION INDOOR AIR QUALITY MANAGEMENT PLAN- 0 pts

EQ CREDIT: INDOOR AIR QUALITY ASSESSMENT- 0 pts

EQ CREDIT: THERMAL COMFORT- 0 pts

All temperature and humidity controlled by ddc system to exact design specifications

EQ CREDIT: INTERIOR LIGHTING- 0 pts

Mostly fluorescents used, mostly automatic controls

EQ CREDIT: DAYLIGHT- 0 pts

No daylighting analyses performed

EQ CREDIT: QUALITY VIEWS- 1 pt

Layout and glazing is such that at least 75% of all regularly occupied spaces in RGE have unobstructed outdoor visibility.

EQ CREDIT: ACOUSTIC PERFORMANCE- 0 pts

No acoustical analysis performed

As evidenced by the previous analysis, the design did not truly aim for any sort of serious LEED certification, despite what the schematic outline states or what the original intent may have been.

Overall System Evaluation

Overall, the system functions very well towards meeting the priorities of the owner, which are running an excellent facility conducive to top-notch biomedical research, while maintaining some level of efficiency and affordability. Given the stringent design conditions, viable system options, and existing conditions, the mechanical design is very reasonable and functions well.

There do however exist potential opportunities for energy savings and cost cuts. If an alternative system for space conditioning were to be used, such as a chilled beam system, it could potentially result in reduced floor-to-floor height, less equipment, and less energy lost to air turnover. Further research will definitely be needed to evaluate whether this strategy can in fact meet air change and other requirements. In addition, given the general lack of energy and equipment analyses, potential exists for improvement in controls and equipment selection.

References

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<u>Appendix</u>

Chvac - Full Commercial HVAC SBM, Inc. Uniontown, OH 44685-8797	Loads Calculation Pro	gram	.		Elite Software Deve Neoucor	n RGE Offices Page 12
Air Handler #1 - R	GE-AHU-3 - T	otal I c	ad Summary	,		
Air Handler Description: Supply Air Fan: Fan Input: Sensible Heat Ratio:	RGE-AHU-3 Variab Draw-Thru with prog 0% motor and fan e 0.87	le Air Volu gram estim fficiency w	ime nated horsepower of vith 0 in. water acros Th	2.38 HP s the fan nis system occi	urs 1 time(s) in the	building
Air System Peak Time: Outdoor Conditions: Indoor Conditions:	1pm in August. Clg: 89° DB, 71° WI Clg: 72° DB, 50% R	3, 90.88 g H, Htg: 75	rains, Htg: 0° DB 5° DB			
Summer: Exhaust controls	outside air, Winte	er: Exhaus	st controls outside ai	ir.		
Zone Space sensible loss: Infiltration sensible loss: Outside Air sensible loss: Supply Duct sensible loss: Return Duct sensible loss: Return Plenum sensible loss: Total System sensible loss:	240,061 0 0 0 s: 0	Btuh Btuh Btuh Btuh Btuh Btuh	0 0	CFM CFM	240,061	Btuh
Heating Supply Air: 240,067 Winter Vent Outside Air (0.0	l / (.957 X 1.08 X 20) 0% of supply) =) =	11,612 0	CFM CFM		
Zone space sensible gain: Infiltration sensible gain: Draw-thru fan sensible gain Supply duct sensible gain: Reheat sensible gain: Total sensible gain on supp	446,398 0 : 5,793 0 0 ly side of coil:	Btuh Btuh Btuh Btuh Btuh			452,191	Btuh
Cooling Supply Air: 452,191 Summer Vent Outside Air (/ (.957 X 1.1 X 17) = 0.0% of supply) =	=	25,265 0	CFM CFM		
Return duct sensible gain: Return plenum sensible gai Outside air sensible gain: Blow-thru fan sensible gain Total sensible gain on retur Total sensible gain on air ha	n: 0 0 n side of coil: andling system:	Btuh Btuh Btuh Btuh	0	CFM	0 452,191	Btuh Btuh
Zone space latent gain: Infiltration latent gain: Outside air latent gain: Total latent gain on air hand Total system sensible and I	67,650 0 0 Iling system: atent gain:	Btuh Btuh Btuh			67,650 519,841	Btuh Btuh
Check Figures						
Total Air Handler Supply Air Total Air Handler Vent. Air (r (based on a 17° TD 0.00% of Supply):):	25,265 0	CFM CFM		
Total Conditioned Air Space Supply Air Per Unit Area: Area Per Cooling Capacity: Cooling Capacity Per Area: Heating Capacity Per Area:	9:		20,043 1.2605 462.7 0.0022 11.98	Sq.ft CFM/Sq.ft Sq.ft/Ton Tons/Sq.ft Btuh/Sq.ft		
Total Heating Required Witl Total Cooling Required Witl	n Outside Air: n Outside Air:		240,061 43.32	Btuh Tons		

Chvac - Full Commercial HVAC Load SBM, Inc. Uniontown, OH 44685-8797	ds Calculation Pro	gram	.		Elite Software I Ne	evelopment, Inc. oucom RGE Labs Page 11
Air Handler #1 - RGE	-AHU-LAB	- Total	Load Sum	mary	/	
Air Handler Description:RGISupply Air Fan:BlowFan Input:0%Sensible Heat Ratio:0.92	E-AHU-LAB Vari w-Thru with prog motor and fan ei 2	able Air Vo ram estima fficiency w	blume ated horsepower ith 0 in. water acr	of 5.46 oss the This sy	6 HP e fan ystem occurs 1 time(s) in	the building
Air System Peak Time:3pmOutdoor Conditions:Clg:Indoor Conditions:Clg:	n in August. : 91° DB, 71° WE : 72° DB, 50% R	3, 86.97 gr H, Htg: 75°	ains, Htg: 0° DB ° DB			
Summer: Exhaust controls outsi	de air, Winte	er: Exhaus	t controls outside	air.		
Zone Space sensible loss: Infiltration sensible loss: Outside Air sensible loss: Supply Duct sensible loss: Return Duct sensible loss: Return Plenum sensible loss: Total System sensible loss:	207,430 0 0 0 0 0	Btuh Btuh Btuh Btuh Btuh Btuh		0 CFI 0 CFI	M M 207,4	30 Btuh
Heating Supply Air: 207,430 / (.9 Winter Vent Outside Air (0.0% o	957 X 1.08 X 20) of supply) =	=	10,03	4 CFI 0 CFI	M M	
Zone space sensible gain: Infiltration sensible gain: Draw-thru fan sensible gain: Supply duct sensible gain: Reheat sensible gain: Total sensible gain on supply sid	1,219,004 0 0 0 0 de of coil:	Btuh Btuh Btuh Btuh Btuh			1,219,0	04 Btuh
Cooling Supply Air: 1,219,004 / Summer Vent Outside Air (0.0%	(.957 X 1.1 X 20 of supply) =) =	57,89	2 CFI 0 CFI	M M	
Return duct sensible gain: Return plenum sensible gain: Outside air sensible gain: Blow-thru fan sensible gain: Total sensible gain on return sid Total sensible gain on air handli	0 0 13,275 le of coil: ng system:	Btuh Btuh Btuh Btuh		0 CFI	M 13,2 1,232,2	75 Btuh 79 Btuh
Zone space latent gain: Infiltration latent gain: Outside air latent gain: Total latent gain on air handling Total system sensible and latent	107,888 0 0 system: t gain:	Btuh Btuh Btuh			107,8 1,340,1	88 Btuh 66 Btuh
Check Figures	and on a 20° TD).	57.90	2 05	NA .	
Total Air Handler Vent. Air (0.00	% of Supply):).	57,09	0 CFN	M	
Total Conditioned Air Space: Supply Air Per Unit Area: Area Per Cooling Capacity: Cooling Capacity Per Area: Heating Capacity Per Area:			33,05 1.751 295. 0.003 6.2	0 Sq.f 6 CFN 9 Sq.f 4 Ton 8 Btul	ft M/Sq.ft ft/Ton ns/Sq.ft h/Sq.ft	
Total Heating Required With Ou Total Cooling Required With Ou	itside Air: itside Air:		207,43 111.6	0 Btul 8 Ton	h ns	

Chvac - Full Commercial HVAC SBM, Inc. Uniontown, OH 44685-8797	Loads Calculation Pro	gram)		Elite Software Deve Ni	lopment, Inc. EOMED CMU Page 8
Air Handler #1 - Cl Air Handler Description: Supply Air Fan: Fan Input: Sancible Heat Patie:	MU-AHU-1 - 7 CMU-AHU-1 Variab Draw-Thru with prog 0% motor and fan e	otal Loac le Air Volume gram estimated fficiency with 0	d horsepower of in. water acros	1.39 HP to the fan	cours 1 time(s) in the	building
Air System Peak Time: Outdoor Conditions: Indoor Conditions:	4pm in June. Clg: 88° DB, 72° WI Clg: 71° DB (avg.), {	3, 97.09 grains 50% RH, Htg:	s, Htg: 0° DB 74° DB (avg.)	iis system o		bunung
Summer: Ventilation controls	s outside air, Wi	nter: Ventilatio	on controls outsi	de air.		
Zone Space sensible loss: Infiltration sensible loss: Outside Air sensible loss: Supply Duct sensible loss: Return Duct sensible loss: Return Plenum sensible loss: Total System sensible loss:	110,832 0 759,475 0 3: 0	Btuh Btuh Btuh Btuh Btuh Btuh	0 9,948	CFM CFM	870,307	Btuh
Heating Supply Air: 110,832 Winter Vent Outside Air (103	/ (.957 X 1.08 X 11) 3.4% of supply) =) =	9,621 9,948	CFM CFM		
Zone space sensible gain: Infiltration sensible gain: Draw-thru fan sensible gain: Supply duct sensible gain: Reserve sensible gain: Total sensible gain on suppl	261,537 0 3,389 0 y side of coil:	Btuh Btuh Btuh Btuh Btuh			264,926	Btuh
Cooling Supply Air: 264,926 Summer Vent Outside Air (1	/ (.957 X 1.1 X 17) = 00.0% of supply) =	=	14,781 14,781	CFM CFM		
Return duct sensible gain: Return plenum sensible gair Outside air sensible gain: Blow-thru fan sensible gain: Total sensible gain on return Total sensible gain on air ha	n: 0 264,166 0 n side of coil: ndling system:	Btuh Btuh Btuh Btuh	14,781	CFM	264,166 529,093	Btuh Btuh
Zone space latent gain: Infiltration latent gain: Outside air latent gain: Total latent gain on air hand Total system sensible and la	31,193 0 372,252 ling system: atent gain:	Btuh Btuh Btuh			403,445 932,538	Btuh Btuh
Check Figures	(based on a 17° TD	\.	14 701	CEM		
Total Air Handler Vent. Air (100.00% of Supply):).	14,781	CFM		
Total Conditioned Air Space Supply Air Per Unit Area: Area Per Cooling Capacity: Cooling Capacity Per Area: Heating Capacity Per Area:	:		14,704 1.0052 189.2 0.0053 59.19	Sq.ft CFM/Sq.ft Sq.ft/Ton Tons/Sq.ft Btuh/Sq.ft		
Total Heating Required With Total Cooling Required With	Outside Air: Outside Air:		870,307 77.71	Btuh Tons		